I. INTRODUCTION

Since the theoretical prediction\textsuperscript{1} and experimental verification\textsuperscript{2-4} of a negative refractive index, the field of electromagnetic metamaterials has experienced enormous growth. The unique properties of metamaterials create possibilities for novel applications difficult to achieve with naturally occurring materials—cloaking\textsuperscript{5-7} and superlensing\textsuperscript{8-10} being two prime examples. Although the aforementioned largely motivate metamaterials research, arguably the real power of metamaterials stems from their ability to construct materials with a specific electric and magnetic response. In practice this is achieved via two different metamaterial unit cells able to independently control the two parameters which govern light-matter interactions in Maxwell’s equations—the electric permittivity ($\varepsilon$) and the magnetic permeability ($\mu$).

The ability to assign optical constants ($\varepsilon, \mu$) to materials greatly facilitates the description of the interaction of electromagnetic waves and matter. However this description is only possible when the wavelength ($\lambda$) is much greater than the element size ($w$), and distances between them ($a$) (i.e., $\lambda > a > w$).\textsuperscript{11} Compliance with these “subwavelength” requirements ensures that electric and magnetic fields vary slowly over the individual elements and therefore experiences an averaged response. The particular microscopic details may thus be ignored and the electromagnetic response may be described as that being due to the optical constants of a homogeneous material in the so called “effective medium regime.”\textsuperscript{12}

However the optical constants are intimately connected to the density of electric and magnetic dipoles within a material. For example the definition of the electrical permittivity is $\varepsilon = \varepsilon_0 (1 + \chi_e)$, where $\varepsilon_0$ is relative permittivity and the electric susceptibility $\chi_e$ describes the relation between the electric field ($E$) and the polarization ($P$), which is equal to the number of electric dipoles per unit volume, that is, $P = p/V = \varepsilon_0 \chi_e E$, where $p$ is the number of electric dipoles, $V$ is the volume, and $E$ is the electric field. A similar definition exists between the magnetic permeability $\mu = \mu_0 (1 + \chi_m)$, and the magnetization ($M$), that is, $M = m/V = \chi_m H$, where $\mu_0$ is relative permeability, $m$ is the number of magnetic dipoles, $\chi_m$ is magnetic susceptibility, and $H$ is the magnetic field. Metamaterials, on the other hand, obtain their electromagnetic response from a combination of their geometry and $p$ and $m$. That is, metamaterial unit cells are well described as effective electric or magnetic dipoles and the true number of dipoles due to the constituent materials is, to first order, not relevant, so long as metamaterials are fashioned from highly conductive structures, and operated below the plasma frequency of the metal. Since it is the metamaterial unit cell that is the effective fundamental dipole one may, by extension, assume that metamaterials should be volumetric in order to appropriately describe their electromagnetic response by effective optical constants.

Metamaterials which extend significantly in three spatial directions are easily fabricated for operation at relatively low rf and microwave frequencies. These may be constructed using printed circuit board techniques thus permitting the assembly of bulk metamaterials. However at terahertz and higher frequencies it is typical to construct metamaterials consisting of a single layer on top of a substrate, owing to the relatively more complicated fabrication processes required—photo, electron beam, and/or focused ion beam lithography. Thus caution must be used when describing the optical constants of metamaterials at terahertz and higher frequencies as these structures do not significantly extend in a third dimension. As such, one must question the assignment of optical constants to all metamaterials which consist of a single or even of several layers.

There have been several works exploring the optical constants of single layer metamaterials,\textsuperscript{13-17} some of which term these structures “metasurfaces.”\textsuperscript{18-20} Most works focus on obtaining $\varepsilon$ and $\mu$ analytically and/or numerically, usually by direct inversion of the transfer matrix equations. Regardless of whether a metamaterial consists of a single or multiple layers, the transfer matrix method permits electromagnetic scattering of a medium of thickness $d$ to be described as\textsuperscript{21,22}

$$ t = \frac{1}{\cos(nkd) - \frac{i}{2}(Z_r + Z_r^{-1}) \sin(nkd)}, \quad (1) $$

$$ r = -\frac{i}{2}(Z_r - Z_r^{-1}) \sin(nkd) / \cos(nkd) - \frac{i}{2}(Z_r + Z_r^{-1}) \sin(nkd), \quad (2) $$
where \( t \) is the transmission coefficient, \( r \) is the reflection coefficient, \( n \) is the index of refraction, \( Z_r \) is the relative impedance, and \( k \) is the wave vector. The refractive index is defined as \( n = c/v \) and the impedance as \( Z = Z_r Z_0 = E/H \), where \( c \) is the speed of light in vacuo, \( v \) is the velocity of light within the medium, \( Z \) is the impedance, \( Z_0 \) is the wave impedance of free space, \( E \) is the electric field, and \( H \) is the magnetic field. However in effective medium theory a connection may be made between the optical constants and the index of refraction and relative impedance, that is, \( n = \sqrt{\varepsilon_r \mu_r} \) and \( Z_r = \sqrt{\mu_r / \varepsilon_r} \). Equation (1) may be inverted to yield explicit equations for the index of refraction and the impedance. We may then also connect these directly to the optical constants, that is,

\[
n = \frac{1}{kd} \arccos \left\{ \frac{1}{2r} \left[ 1 - (r^2 - t^2) \right] \right\} = \sqrt{\varepsilon_r \mu_r},
\]

(3)

\[
Z_r = \sqrt{\frac{(1 + r)^2 - t^2}{(1 - r)^2 - t^2}} = \sqrt{\frac{\mu_r}{\varepsilon_r}}.
\]

(4)

An outstanding question in metamaterials research is under what conditions the right side of Eqs. (3) and (4) are valid.\textsuperscript{23} In this paper we investigate the cases under which single layer metamaterials may be described by the optical constants, thus satisfying Eqs. (3) and (4). Two different structures are studied, each with two different layer thicknesses, in order to demonstrate various prototypical results. A series of simulations and experiments are performed in order to clarify the dependence of the optical constants on metamaterial layer thickness.

II. DESIGN AND FABRICATION

We present two electric split ring resonator structures\textsuperscript{24–27} in single and multilayer configurations, which we term ERR1 and ERR2, see Fig. 1. For both structures, the in-plane size of the unit cell is \( 50 \mu m \times 50 \mu m \), and both the width and height of the metamaterial is \( 36 \mu m \), with a line width of \( 4 \mu m \). The capacitive gaps, found in the middle of the ERR2 structure and on the sides of the ERR1 structure, are \( 4 \mu m \). The metallic metamaterial layer is a 150-nm-thick layer of gold and is embedded (centered) within the substrate material, polyimide, giving a total unit cell thickness of either 50 or 15 \( \mu m \), see Fig. 1. We term these two configurations as type 50 and type 15 based on their unit cell thickness. Each of these individual metamaterial unit cells (ERR1 and ERR2) of both substrate thicknesses (type 50 and type 15) are then stacked and we study \( n = 1, 2, 3, \) and \( 4 \) layers of both structures and both types. Thus a total of 16 different metamaterial samples are computationally and experimentally investigated.

Samples were fabricated with the dimensions shown in Figs. 1(a) and 1(b) for ERR1 and ERR2, respectively. The structures were fabricated on layer-by-layer films of polyimide (PI-5878G HD Microsystems TM). Substrate thicknesses between adjacent metallic gold layers are chosen as mentioned above. Here we take the 50 \( \mu m \) ERR1 as the reference for demonstration of the fabrication process. First a 25 \( \mu m \) layer of polyimide was spin coated on a silicon substrate and cured at 275°C in an \( N_2 \) environment for 5 h. Then the 150-nm-thick gold metamaterial was fabricated and patterned using optical lithography and lift-off techniques. For better pattern transfer, vacuum contact mode was used during the exposure process. Substrate thickness is accurate to \( \pm 1 \mu m \). For samples with more than one layer, a second metamaterial layer was patterned in the same manner as the first. Alignment between the two layers was performed with a mask aligner which has an accuracy of 0.5 \( \mu m \). Additional layers of 50 \( \mu m \) polyimide and 150 \( \mu m \) gold can be coated and patterned in the same way. For the last layer, a 25-\( \mu m \)-thick layer of polyimide was coated on top. In the final step, the entire multilayer sample, encapsulated in polyimide, was peeled off the silicon substrate, thus yielding a free-standing metamaterial multilayer structure embedded within the host dielectric material.\textsuperscript{28}

III. SIMULATION AND EXPERIMENT

The structures were simulated with a commercial finite time domain solver, CST Microwave Studio. The metamaterial itself was modeled as lossy gold with a conductivity of \( \sigma_0 = 4.56 \times 10^7 \) (S/m). The embedding dielectric had a frequency independent lossy dielectric of \( \varepsilon_r = 2.89 + 0.08i \). ERR1 and ERR2 are designed to have resonances at 0.76 and 1.07 THz, respectively. In Fig. 2 we show the dependence of the metamaterial resonance frequency (for a single layer) on layer thickness (d) in the propagation direction, that is, in the direction of \( \mathbf{k} \) (see Fig. 1). In all cases, the metamaterial lies in the center of the dielectric layer. Dashed vertical lines at two different thicknesses show that, for both structures, the resonance frequency is continuing to change as a function of layer thickness for 15 \( \mu m \), but is saturated for 50 \( \mu m \). We simulated all 16 metamaterial samples and performed extraction of the optical constants for each using Eq. (2). For the four layer metamaterial structure, with each layer being 50 \( \mu m \), the total thickness of the film is 200 \( \mu m \). With a resonance frequency for ERR1 (ERR2) of \( \omega_1 = 0.76 \) THz...
(ω2 = 1.07 THz), the corresponding resonant wavelength of λ1 = 395 (λ2 = 280) μm is comparable to its thickness.

Fabricated samples were experimentally characterized using terahertz time-domain spectroscopy (THz-TDS), which permits amplitude and phase measurements of the transmitted electric field. A reference measurement was also characterized (open channel), thus permitting determination of absolute transmission coefficient. Experimental data for all samples and reference measurements was collected over 25 ps. The complex transmission coefficient permitted us to calculate the frequency dependent dielectric function through inversion of the Fresnel equations. Etalons resulting from multiple reflections within the metamaterial were incorporated into the extraction algorithm.29,30

IV. RESULTS

The transmitted electric field for each metamaterial ERR1 and ERR2 is shown in Figs. 3(a) and 3(b) for a polyimide layer thickness of 50 μm. We take the single layer ERR1 sample [black curve Fig. 3(a)] as a point of discussion, which yields 90% transmission at 200 GHz and at a frequency of 1.2 THz is about 80% transmissive. A minimum of 40% is observed at about 0.75 THZ and the curve is otherwise featureless. Transmission for the other type 50 ERR1 samples also each show minima near 0.75 THz with values of 12%, 5%, and 0.1% for n = 2, 3, and 4 layers, respectively. Notice that, unlike the n = 1 thick ERR1 transmission, other samples show oscillatory behavior beyond just the minimum near 0.75 THz. For example the n = 2 thick ERR1 sample (red curve), shows a local minimum of 72% at 450 GHz and a local maximum of 80% at 675 GHz. This local maximum seems to shift lower for an increase in the number of layers, that is, 500 GHz for n = 3 and 425 GHz for n = 4 layers. This trend is also observed for the ERR2 metamaterial.

ERR1 with a 15-μm-thick substrate (type 15), on the other hand, yields a transmission which does not seem to follow the same trend. For example the n = 1 layer shown in Fig. 4(a) shows a transmission minimum near 0.8 THz followed by maximum of 83% at 1.0 THz. The n = 2 and n = 3 layers are not so different with the maximum moving nonmonotonically to 0.95 and 0.98 THz. In the n = 4 sample a local minimum and maximum of 60% and 62% appear at 0.45 and 0.6 THz, respectively. The 15-μm-thick ERR2 sample has roughly the same transmissive behavior.

In Figs. 3(c) and 3(d) the simulated transmissions are shown for 50-μm-thick ERR1 and ERR2, respectively. We achieve good agreement between simulated and experimental transmission, that is, characteristic frequency-dependent features discussed above for the experimental results are all observed in the simulated transmission. Although the value of transmission maxima in the experimental and computational curves is similar, there is discrepancy in the minima. For example, the simulated minimum for n = 1 layer thick ERR1

FIG. 2. (Color online) Dependence of the resonant frequencies of ERR1 (blue symbols) and ERR2 (red symbols) (single layer structures) on the embedding substrate thickness.

FIG. 3. (Color online) Experimental and simulated transmission coefficient for type 50 metamaterials. ERR1 is shown in (a) and (c) and ERR2 in (b) and (d).

FIG. 4. (Color online) Experimental and simulated transmission coefficient for type 15 metamaterials. ERR1 is shown in (a) and (c) and ERR2 in (b) and (d).
sample (black curve) shown in Fig. 3(c) is 25% compared to a value of 40% for the experimental curve [black curve in Fig. 3 (a)]. A similar disagreement is found for all transmission data presented in Fig. 4.

The refractive index and the impedance of each configuration can be determined from the amplitude and phase of the transmitted electric field, see Eq. (1). For the electric metamaterials studied here, the structure is composed of two combined split ring resonators with identical sizes facing either inward or outward within a single unit cell. Magnetic coupling is thus forbidden by symmetry and the electric response dominates. We thus take the relative permeability \( \mu_r = 1 \) for each configuration such that the dielectric function can be obtained from Eqs. (3) and (4). Despite the periodic nature of multilayer samples, we take their total thickness to account for the relative difference in phase (compared to a reference pulse), for example, the phase change for a \( n = 2 \) type 50 sample is calculated over 100 \( \mu m \). The experimentally determined dielectric function for metamaterial samples with 50-\( \mu m \)-layer thickness are presented in Figs. 5(a) and 5(b).

The permittivity for ERR1 and ERR2 shows Lorentz like oscillators centered at \( \omega_1 = 0.75 \) THz and \( \omega_2 = 1.05 \) THz, respectively. As can be observed, there is little change in the permittivity for each sample for all layer thicknesses. There is, however, a discrepancy between the \( n = 1 \) metamaterial and others for both ERR1 and ERR2.

Figure 5 shows the simulated results for ERR1 (c) and ERR2 (d) with a substrate thickness of 50 \( \mu m \). Four different simulations are presented for each metamaterial, where the black, red, green, and blue curves are for \( n = 1, 2, 3, \) and 4 layers thick, respectively, in the propagation direction. As can be observed, the extracted dielectric function for all metamaterial single and multiple layer structures are identical, with no change in oscillator strength or central frequency location.

In order to elucidate the nature of the above results, we also simulated and characterized the dielectric function for both ERR1 and ERR2 for a different substrate embedding thickness of 15 \( \mu m \) (type 15). Figure 6 presents results of this investigation where (a) and (b) shows the frequency dependent permittivity for both metamaterials and (c) and (d) show the corresponding simulations. It can be observed that the permittivity is seen to change for an increasing number of layers, from one to four (black, red, green, and blue curves). Specifically, for both ERR1 and ERR2, the resonance frequency red shifts and the maximum peak amplitude decreases for multiple layers. Small variations in peak amplitude and peak position for each configuration are observed.

V. DISCUSSION

It is evident that the optical constants, displayed in Figs. 5 and 6, for type 50 and type 15 samples behave differently, although they are comprised of the exact same metamaterial geometry (for both ERR1 and ERR2). As shown in Fig. 2, the resonant frequency of these metamaterials continually shifts to lower frequencies as a function of layers thickness, until finally asymptoting around 50 \( \mu m \). For the 50-\( \mu m \)-thick samples, the saturated resonance indicates that the substrate is of sufficient thickness and dielectric constant such that there is negligible interaction between adjacent metamaterial layers. This shows that the electromagnetic response within a unit cell can be treated as a homogenous response, that is, in the effective medium limit, and is independent of the number of layers. Thus in the type 50 case we may define a set of optical parameters for the single layer metamaterial which is equivalent to a bulk response.

In contrast the 15-\( \mu m \)-thick samples yield significant interaction between adjacent unit cells, owing to the relatively thin substrate and dielectric value. When stacking multiple
cells, the range of the layer-to-layer coupling exceeds the unit cell thickness and neighboring unit cells interact. Unlike the previous case, it would not be correct to describe a single layer 15-μm-thick sample by a set of optical constants, as \( \epsilon(\omega) \) depends upon the number of layers. In our studies the response seems to saturate above six layers (not shown) for the type 15 metamaterials.

Our computational investigations suggest that metamaterials consisting of only a single layer may or may not be describable by the optical constants \( \epsilon \) and \( \mu \). This depends on some key parameters, namely the embedding dielectric thickness, the complex dielectric constant of the embedding dielectric, the filling fraction, and the particular type of metamaterial geometry, that is, the symmetry point group and its relation to incident radiation.\(^3\) A nonchanging, layer independent, permittivity in the 50-μm-thick samples (type 50) versus a gradually red-shifting permittivity in the 15-μm-thick samples (type 15) is observed. Although this is clear in simulation it is apparent that there is some discrepancy for experimental measurements of single layer structures, both for type 50 and type 15 metamaterials. All experimental and simulated transmittance data (Fig. 3) match well, but the experimentally determined permittivities between the two cases (type 50 and type 15) is not as prominent as expected. This discrepancy can be attributed to the relatively weak mechanical strength of polyimide single layer films.

A thin polyimide film, although well characterized by optical constants,\(^2\) is highly flexible, mechanically weak, and not self-supporting. In the single layer case the as measured films surface is slightly modulated resulting in undesirable effects. We find that surface wrinkling leads to a nonuniform lattice parameter which presents itself as inhomogeneous broadening and thus a reduction in oscillator strength [black curves in Figs. 5(a) and 5(b)]. In transmission this results in a lower absorptive feature and thus higher transmission. For example it can be observed that the disagreement between experimental and simulated transmission \( \Delta T = T_{\text{exp}} - T_{\text{sim}} \) (Figs. 3 and 4) is worse for single layer metamaterials but gradually improves with more layers. If we take the minimum in transmission as our point of evaluation we find \( \Delta T = 18\% \) for single layer type 50 films. With the addition of more metamaterial layers an increase in mechanical strength is achieved and significantly less surface fluctuations were observed in the measurements of multilayer configurations for both 15 and 50-μm structures. Indeed \( \Delta T \) diminishes for \( n = 2, 3, \) and 4 layers and is 10%, 6%, and 1%, respectively.

Simulated results shown for the type 15 structures indicate that a significant red shifting of the dielectric function occurs, due to interlayer coupling. As a result the optical constants of the 15-μm-thick metamaterial samples depend on the number of layers. Type 15 metamaterials achieve a more complicated and undesirable response compared to type 50 (50-μm-thick) metamaterials. Although this may often be an unplanned interaction, this effect has been utilized in some cases to achieve unit cells with both electric and magnetic response.\(^4\) Other examples include electromagnetic inducted transparency\(^9\) and energy level hybridization.\(^9\) It should be stressed that in order to define optical constants for a single layer metamaterial, any interactions that may occur due to the addition of other materials in proximity to the surface should be minimized.

As the optical constants of the type 50 single layer metamaterials explored here are equivalent to bulk, we may calculate the number of electric dipoles involved in the electric responses shown here. Lorentz oscillators are fit to the simulated data, shown in Figs. 5 and 6, and described by

\[
\epsilon(\omega) = \epsilon_\infty + \frac{\omega_p^2}{\omega_0^2 - \omega^2 - i\gamma\omega},
\]

where \( \omega_0 \) is the center frequency of the oscillator, \( \epsilon_\infty \) is the dielectric constant at frequencies much greater than \( \omega_0 \), \( \gamma \) is the damping, and \( \omega_p^2 \) is the square of the plasma frequency given by

\[
\omega_p^2 = \frac{ne^2}{\epsilon_0 m},
\]

where \( n \) is the number density (number of charges per unit volume \( n = N/V \)) involved in the oscillation, \( e \) is the charge of an electron, and \( m \) is the mass of an electron.

We may also connect the number of charges \( N \) involved in the metamaterial resonance to the electric dipole \( p \) from assuming a form for the electric dipole moment of

\[
p = -N ed,
\]

where \( d \) is the metamaterial gap of 4 μm. Table I lists the parameters of Lorentzian fits to the dielectric functions of type 50 ERR1 and ERR2, including the calculated number of charges \( N \) determined from Eqs. (5)–(7) and using a volume of \( V = L^3 \) where \( L = 50 \mu m \) for type 50 metamaterials.

As a general prescription for use of the optical constants for single layer metamaterials one may proceed as follows. First systematically explore the scattering parameters (or effective dielectric properties, e.g., resonance frequency) of single layer metamaterials as a function of embedding dielectric thickness. Once this parameter asymptotes to a steady-state solution one can be sure the fields (electric and magnetic) have diminished to the point that any material placed at the metamaterial boundary will not affect its electromagnetic properties. Thus all the microscopic details of the single layer metamaterial may be ignored and considered to be truly homogenized and well described by the optical constants.

**VI. CONCLUSION**

We have computationally and experimentally explored the conditions under which single layer metamaterials may be described by bulk optical constants. Two types of electric...
metamaterials were explored, both with two different sizes of embedding dielectric. The type 50 configuration was a cubic unit cell with a lattice parameter of 50 μm, and the type 15 configuration was a tetragonal unit cell, with dimensions 50 × 50 × 15 μm³. The tetragonal metamaterials were shown to yield layer dependent optical constants, whereas the cubic type 50 metamaterials yielded layer independent optical constants. A Lorentz oscillator model was fit to type 50 metamaterials which permitted determination of the total number of charges involved in the primary metamaterial resonance.

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